Mitigating Electromagnetic Interference on PCB in Electric Vehicles: A Review

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Abstract: The increasing integration of electronic equipment in electric vehicles (EVs) compared to traditional vehicles significantly elevates the challenges posed by electromagnetic interference (EMI) to the functionality of printed-circuit boards (PCBs). This paper provides a comprehensive review of recent advancements in the field of PCB electromagnetic compatibility (EMC) in EVs. By examining the principle of EMI generation and conduction, as well as EMI sources within EVs, the article identifies its specific impacts on PCB. Moreover, mitigative solutions are proposed, including the suppression of primary EMI sources, the implementation of shielding techniques, and EMC-oriented PCB design. In the end, this paper analyzes the feasibility of each solution, and provides recommendations for future research in this area.

Keywords: Electric vehicles, Printed-circuit-board, Electromagnetic interference, Electromagnetic compatibility

1. Introduction

Electric vehicles (EVs) offer numerous advantages over traditional vehicles, including reduced emissions, enhanced energy efficiency, and lower operating costs. The global adoption of EVs is accelerating, with sales projected to reach approximately 17 million by the end of 2024, representing over 20% of global car sales, understanding their growing popularity. [1]. Printed-circuit-board (PCB) is the core of the EV operating system, which serves as the foundation of electronic systems [2]. PCB plays a crucial role in integrating and managing a large number of electronic components that are essential for functions ranging from power distribution to vehicle control systems.

Electromagnetic interference (EMI) affecting PCBs in EVs primarily originates from two sources: the vehicles' motor drive system and internal PCB circuitry. Strong EMI can lead to signal distortion and cause the malfunction of the PCB. In such cases, electronic equipment can negatively influence

each other, affecting the normal operation of electronic equipment and instruments. In serious situations, this can threaten the operational safety of EVs.

Mitigating EMI enables the automobile PCB to better transmit signals and data, reduce signal loss and interference, improve electromagnetic compatibility (EMC), and degrade radiation levels [3]. The mitigation of EMI is essential for improving the maneuverability, acceleration, and overall performance of the vehicle. Through the design and production of high-quality PCB, the normal operation and coordination of these safety systems can be ensured, thus providing vehicle stability, brake safety, and occupant protection. Currently, research on the analysis and optimization of electromagnetic interference in electric vehicles focuses mostly on the interference source and propagation path, with a lack of research on protective solutions for individual sensitive devices such as PCB on EVs.

This paper reviews the current state of research and assesses the feasibility and effectiveness of various EMI mitigation strategies. Section II presents the principle of EMI generation and dissemination, the source of EMI in EVs and the impact of EMI on PCBs. In Section III, effective solutions from the three perspectives are presented—suppressing the generation of EMI from noise sources, reducing EMI on EMI propagation paths, and optimizing PCB design. In addition, advantages and disadvantages of the above methods are discussed, along with possible application scenarios. By integrating these insights, this article aims to provide feasible suggestions for ensuring the efficient and stable work of PCB in EVs and improving the reliability, efficiency and safety of EVs.

2. Electromagnetic interference in electric vehicles

Electromagnetic interference (EMI) refers to the interference effect of electromagnetic waves generated by electromagnetic induction effect on other electric devices in the environment during the normal operation of electric devices or systems. The two types of EMI are radiation emission (RE) and conducted emission (CE), depending on the electromagnetic interference's transmission channel. The transmission path of CE includes wires or common ground wires, which can be transmitted through space radiation or near-field coupling. RE is generally transmitted in space in the form of electromagnetic coupling, and shielding materials are used to prevent or reduce energy transmission in space.

The drive system of electric vehicles (EVs) is the main source of EMI of EVs, consisting of highpower electric devices, including power batteries, high-power DC/DC converters or DC/AC inverters, drive motors and their connected high-voltage cables. When these power electric system work, it will emit strong electromagnetic interference, forming a complex electromagnetic environment. During the breaking process of the switching element, due to the jump in voltage and current in a short period of time, the $\frac{du}{dt}$ of many switching elements reaches tens of thousands of volts per microsecond, and the operating frequency of the switch also reaches tens of kilohertz, thus forming strong radiation and conductive electromagnetic interference. On the other hand, high-voltage cables are used to link the power drive components. When operating, a significant amount of current—hundreds of amps flows, and the variations in that current generate a strong electromagnetic radiation. When these EMI noises spread, they can influence various electric devices and receivers installed in EV systems, resulting in malfunctions or performance degradation. The block diagram of the plug-in hybrid electric vehicle (PHEV) configuration is depicted in figure.1 [4].

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Figure 1: PHEV configuration [4]

In addition, the PCB will be interfered with and emit electromagnetic radiation internally. According to the basic theory of electromagnetic field, when there is RF (radio frequency) current in the external transmission line or PCB printed line, the current from the current source to the load must be returned to the current source through the return path, so that the formation of a closed current loop will generate a magnetic field, which will also generate a radiation electric field, and then form EMI[5.6.7]. The key to the electromagnetic compatibility design of PCB is how to reduce radiation ability and how to improve anti-interference ability. Reasonable layout and wiring are the guarantee of the design of the PCB.

3. Mitigative solutions

3.1. Suppressing main electromagnetic interference sources

Unlike traditional engine vehicles, electric vehicles integrate a number of high-voltage components. This section will focus on how to prevent these components from generating EMI interference sources. For switched-mode power supply, technologies such as parallel capacitive coupling, frequency hopping, and digital active EMI filtering have been identified as effective solutions to reduce high-frequency noise and improve system stability. In the context of CAN bus interference, the use of electrical isolation means and shielded twisted pair is essential to maintain data transmission integrity and reduce overall system outages. In addition, suppressing the EMI of the low-voltage battery pack is also an important part. By implementing these strategies, engineers can achieve a higher level of interference control, resulting in stronger and more stable electronic systems within electric vehicles.

3.1.1. Suppression of electromagnetic interference from Switched-Mode Power Supply (SMPS)

3.1.1.1. Parallel capacitive coupling (Cx)

The switching operation of DC/DC converters generates significant EMI, especially during the start and brake phases. These conditions place high load requirements on switching power supplies, resulting in increased interference levels on positive high-voltage power lines [8].

If we want to tackle this EMI issue head-on, we need to focus on dealing with specific frequency resonators, like the troublesome 2 MHz one. By eliminating or reducing the resonant amplitude of 2 MHz, the conduction voltage can be controlled within an acceptable range. Reducing equivalent parasitic inductance Ls of the DC filter capacitor C_{DC} is to make the resonant point shift from 2 MHz

to a high frequency band of about 10 MHz. Here we can choose a parallel 1uF X capacitor C_X and C_{DC} , and its parasitic inductance L_{CX} is 10nF, as shown in Fig 2 [9].



Figure 2: Filter circuit to reduce the peak of the resonance point at 2MHz

The advantage of using this method to design the filter circuit on the PCB of the DC-DC converter is: mitigating the electromagnetic coupling between the filter input and output cables; The design size is significantly reduced to only about one-fifth of the high-voltage filter (as shown in Fig 3), greatly simplifying engineering design.



Figure 3: Filter circuit on the PCB

3.1.1.2. Add the frequency hopping technique

Through manipulation of the switching signal frequency, it becomes possible to minimize the peak of the power spectrum. The integration of a frequency hopping control module into the traditional DC-DC converter schematic enables precise control over the generation of sawtooth waves at varying frequencies. The frequency of these sawtooth waves dictates the central switching frequency of the DC-DC converter. Scanning through 8 different switching frequencies theoretically reduces the power spectrum at the DC-DC converter output node by up to 18 dB [10].

3.1.1.3. Digital Active Electromagnetic Interference Filtering (DAEF) technique

The Digital Active EMI Filtering (DAEF) technique represents a groundbreaking advancement in SMPS conducted EMI suppression technology. This paper [11] introduces a novel DAEF topology that possesses the capability to effectively suppress both common mode (CM) and differential mode (DM) EMI while preventing any conversion between them. The DAEF topology planning is shown in Figure 4. It includes electromagnetic interference signal detection circuit, ADC sampling circuit, DAC output and decoupling circuit between injection point and sensing point, the DAEF system stands as a versatile solution for EMI mitigation and management.

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Figure 4: General scheme of proposed DAEF

The electromagnetic interference detection circuit is an RC high-pass filter composed of resistance and capacitance. By designing decoupling circuit, the coupling between signal sensing point and signal injection point can be effectively reduced. The electromagnetic interference injection circuit can be partially designed by an RC low-pass filter. Integrating the DAEF controller into the inherent controller of the power converter proved to be a cost-effective solution, ultimately reducing the overall expenses associated with the power converter. In addition, placing a high-impedance RF inductor as a decoupling circuit between the injection point and the induction point can effectively reduce the coupling between the two points and further improve the filtering performance.

3.1.2. Suppression of electromagnetic interference from CAN bus

In addressing the suppression of EMI from the CAN bus, it is essential to fortify each node's antiinterference capabilities. Opting for a CAN repeater, a CAN interface card with photoelectric isolation, and a CAN/485 conversion module allows for electrical isolation of network terminal equipment. This isolation prevents any discrepancies in reference ground potential from impacting other devices, ensuring that interference does not infiltrate the control circuit and thereby safeguarding the control system's integrity [12].

3.1.3. Suppression of electromagnetic interference from low voltage battery pack

This study presents an embedded DAEF that can be seamlessly integrated into digital controllers of DSP-based DC converters designed for low-voltage battery pack charging in electric vehicles. Figure 5 depicts the layout of the Converter closed loop block diagram, which consists of two digital control loops embedded in the DSP device, each of which acts on the power converter.[13]

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Figure 5: Converter closed loop block diagram

3.2. Reducing electromagnetic interference noise on propagation paths

The above section has introduced three methods for suppressing main EMI source, cutting off the EMI propagation path is also important way to mitigate EMI.Shielding techniques are main method of cutting off the EMI propagation path, Figure.6[14] shows the mechanism of EMI shielding, EV's internal High-current components and weak current components need different shielding methods, high-precision equipment inside EVs such as driving computers, the control signal of this equipment is relatively weak, Usually it uses metal shell shielding technology, some additional charging devices, traditional wired charging pile and wireless charging pile, These high-power equipment will interfere with the electronic equipment in EVs, now it can be shielded with aluminum plate, this section reviews the traditional feasible methods used on EVs such as metal shell shielding and high-current and weak current separation shielding techniques, but also puts forward some small number of popular or gradually put into use methods, these methods have good prospects for development, such as high-permeability magnetic materials, Ferrite applications in EVs.The following table.2 shows the methods of reducing EMI noise on propagation paths.

	Methods	References
Shielding Techniques	Metal Shell Shielding	[15,16]
	Ferrite Shielding for Wireless	[17]
	Power Transmission	
	Multilayer Shielding	[18-20]
Suppression of EMI from Motor Drive System	Using X and Y Capacitors	[21]

Table 1: approaches of reducing EMI noise on propagation paths

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Figure 6: EMI shielding mechanism based on transmission line theory [14]

3.2.1. Shielding techniques

3.2.1.1. Metal shell shielding

Metal shell shielding techniques are traditional and in EVs they are widely used, conductive cavity can be applied to protect the sensitive equipment in EVs. The purpose of metal shell shielding is to prevent the external electric field from entering a specific area and place the cavity conductor. Under the action of the external electric field, the surface charge of the metal parts will be redistributed until the internal field strength is zero everywhere. The use of grounded closed metal shell as a cavity conductor to shield the external electric field is a good electrostatic shielding method in EVs, usually metal shell with low resistivity metal materials such as aluminum [15] or iron aluminum alloy, in EVs, metal shell is not fully closed, the shell has holes. Although it can also play a role in electrostatic shielding, it destroys the conductive continuity of the shield, and non-conductive gaps or holes may lead to electromagnetic leakage and electromagnetic pollution.

3.2.1.2. Ferrite shielding for wireless power transmission

Static magnetic field is the magnetic field generated by constant current or permanent magnet, low frequency magnetic field shielding refers to the low impedance shielding cavity and protection space used in parallel, low frequency magnetic field always tends to preferentially pass through the low impedance shielding cavity, thus protecting the device in the protection space, the use of iron, nickel and other high permeability magnetic alloy made of shielding cover, is the traditional magnetic field shielding practice, but compared with electrostatic shielding, The difference between the conductivity of ferromagnetic material and air is much smaller, magnetic shielding will always produce some magnetic leakage, although the use of multi-layer shielding to achieve a better shielding effect, but the magnetic shield becomes more bulky, affecting the driving effect of electric vehicles. Most EVs use aluminum plates between the transmitter and receiver of the wireless charging system to shield the magnetic field. In a study on the application of ferrite [17] as a magnetic field shield material in the wireless power transmission system, the advantages of ferrite compared with traditional magnetic field shield materials were demonstrated, and the magnetic field shielding effect of the wireless power transmission system was improved.

3.2.1.3. Multilayer shielding

MXene, a new family of 2D materials, has been found to have excellent electromagnetic shielding properties due to its excellent electrical conductivity, MXenes has a higher dielectric mass than graphene [18], so they have stronger conductivity, and the porous structure of MXenes [19] has better EM absorption capacity than the layer structure. This article analyzes the present study of MXene and graphene applied to porous composites, a benefit of using multilayer shielding is that reflections can be minimized, and as the number of layers increases, the shielding efficiency of EMI can be increased to more than 80dB [20].

3.2.2. Suppression of electromagnetic interference from motor drive system

The conducted emissions from the motor driving system can disrupt other systems in electric vehicle. Addressing this issue, the paper [21] proposes a series of low-cost EMI mitigation techniques.

To mitigate EMI from the high-voltage (HV) parts in the motor driver system, the use of X and Y capacitors is recommended.

X capacitors and Y capacitors are important safety capacitors in power electronic equipment, which are used to eliminate common mode interference and EMI in power grids, respectively. X capacitor is mainly used to filter and reduce the influence of high-frequency noise on the circuit to ensure the stable operation of the equipment; The Y capacitor mainly inhibits the common mode interference, improves the anti-interference ability of the equipment, and ensures the safety of use in the ground circuit. In Figure.7[21], two Y capacitors are deployed for each HV port to filter common-mode noise, while an X capacitor is employed to address differential-mode noise. These capacitors function effectively as first-order filters and are implemented at a low cost without the need for inductors.



Figure 7: EMI path of the common mode and differential mode [21]

The implementation of this measures can enable EMI measurements to meet the requirements of CISPR 25 Level III and even level V in some frequency bands.

The first two parts have introduced feasible EMI mitigation methods from suppressing main EMI source and cutting off EMI propagation paths, the next part will cover some methods to mitigate EMI from PCB design perspective.

3.3. PCB electromagnetic compatibility design

Compared to other electric devices such as electric motor system and batteries, the PCB produces relatively low levels of EMI. However, due to the small scale of PCB, even this small amount of EMI can have a significant impact on PCB itself. To address this problem, this section summarizes the

methods to mitigate EMI noise in EVs. Generally, the mitigation techniques can be classified into two primary categories. The following table outlines the approaches along with their references.

	Methods	References
Layout and Routing	High-Frequency Signal Line Arrangement	[12,23,24]
	Component Layout	[23,25-27]
	Power Plane Design	[12,26,28-31]
	Stack-up Design	[28,34]
	Via (Via-hole) Design	[32]
Grounding	Reduce Ground Line Impedance	[26,35,36]
	Ground Plane Position and Design	[35,37]

Table 2: Approaches of PCB EMC design

3.3.1. Layout and routing

Improper layout or routing is the major cause of electromagnetic interference, particularly in digital analog hybrid layouts [22]. Therefore, proper layout and routing are crucial for reducing EMI.

When integrating low-speed, medium-speed, and high-speed circuits, it is crucial to separate lowlevel analog circuits from digital circuits as much as possible. This layout shortens the path of highfrequency currents on the printed circuit board (PCB), which helps mitigate the noises within the board [23].

EMI issues in PCB mainly include common impedance coupling, radiation from high-frequency signal lines, crosstalk and the induction of high-frequency radiation by printed traces [22]. Among these, radiation from high-frequency current-carrying lines has the most severe impact, so special consideration should be given to the placement of high-speed signal transmission lines during layout and routing. Here are some common principles for routing:

3.3.1.1. High-frequency signal line arrangement

PCB routing should avoid the crosstalk caused by close parallel routing of signal lines, especially the clock lines, as they usually have the highest frequency [23]. If parallel routing cannot be avoided, the distance between parallel signal lines should be increased. If the space between signal lines reaches 3W (W is the width of the signal line) 70% of crosstalk issues can be eliminated, while spacing them at 10W can eliminate 98% [24]. If two signal lines are close together, a ground line should be routed between them, or large area copper ground should be laid on adjacent layers to reduce inter-line crosstalk. Additionally, high-frequency signal lines should use smooth arcs and avoid using 90-degree bends to minimize reflections caused by abrupt changes in the he transmission line's characteristic impedance [23].

Because the clock lines usually have the biggest EMI impact, special method is needed. By adding magnetic beads, clock interference signals on the PCB can be suppressed. These beads are heated to dissipate the high-frequency current. Filtering ability of the bead is related to the frequency, material, bead size and the current. The principle behind choosing beads for EMI suppression is that they have the highest impedance at EMI noise frequencies. Different types of magnetic beads can be selected according to specific design requirements [12].

3.3.1.2. Component layout

Closely related components should be placed together to keep high-speed lines as short as possible. For high-current components such as relays, indicator lights, and speakers, their ground lines should be routed separately to reduce noise on the ground lines [23]. Increasing the distance between components that generate strong radiation electromagnetic fields and those sensitive to electromagnetic induction is an important way to reduce interference between components on the PCB. Additionally, the crossing of high and low voltage components and strong and weak signal components should be avoided [23,25]. If small signal amplifiers are equipped on the board, the weak signal lines before amplification should be kept away from strong signal lines and, if possible, shielded by ground lines [26]. Furthermore, components that generate magnetic fields, such as transformers, speakers, and inductors, should be oriented to reduce the amount of the printed conductors that cut into the magnetic field lines. The magnetic field directions of adjacent components should be perpendicular in order to minimize mutual coupling.

To minimize the effects of overheating, high-power transistors, high-power ICs, and high heatgenerating components should be positioned in easily heat-dissipating areas [26]. As for crystal oscillators, they should be placed as close to integrated circuits as possible, and crystal oscillator case should be grounded [23,27].

3.3.1.3. Power plane design

The power layer shall be adjacent to and below the ground layer. Each power supply pin should have a decoupling capacitor of 0.01F to 0.1F, and the decoupling capacitor should be placed as close to the individual pins as possible [28]. The inclusion of decoupling capacitors in the lower power layer can introduce additional charge reservoirs to compensate for potential signal voltage dips, thus mitigating the impact of switching noise [29]. Moreover, minimizing the distance between the noise source and the decoupling capacitor is also an effective meethod for ensuring good signal trasmission [29].

Reference [12] proposes a decoupling capacitor selection method based on geometric average resonance points. When two different capacitors are connected in parallel, two anti-resonant points and one resonant point appear on the impedance curve, as shown in Figure.8. The received self-resonant frequency of the decoupling capacitor can be equal to the average frequency of two adjacent anti-resonant points where the decoupling capacitor is placed. By calculating the geometric mean of these three points, the minimum impedance peak on the impedance curve can be found and the appropriate decoupling capacitance can be selected. With regard to the placement of decoupling capacitor should not exceed the decoupling radius of the capacitor.



Figure 8: Impedance curve of two different capacitors in parallel [12]

The electric field between the power plane and ground plane is variable, causing electromagnetic interference radiation at the edge of the board, known as the edge effect, as shown in Figure.9. Pull back one of the planes can reduce edge effect. Retracting the power plane by 20H (H is the dielectric thickness between the power and ground planes) can confine 70% of the electric field within the ground edge while retracting by 100H can confine 98% [26,30,31]. (Figure.10)



Figure 9: Coupling along PCB edge [31]



Figure 10: Edge emission with retracing design [31]

3.3.1.4. Stack-up design

Stack-up arrangement is also a factor affecting PCB EMC. To ensure good electrical performance, cross-section of each routing layer must be well-designed [28]. The layer stack should follow symmetry principles. The distance between the power plane and its corresponding ground plane should be minimized to form an effective planar capacitor., reducing power plane impedance [34]. Figure.11 shows a schematic of symmetrical layer stack design.

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Figure 11: A stack-up solution [38]

All signal layers should be adjacent to their corresponding ground planes, avoiding adjacency of two signal layers [34]. Symmetrical layering design can eliminate open edge effects, which confines resonance energy to the power-ground plane. The copper plating process can connect the edges of two ground planes, thus eliminating open edges [34]. Figure.12 shows the schematic of symmetrical layer stack design and reducing electromagnetic interference by eliminating open edges.



Figure 12: Symmetrical layering design [34]

3.3.1.5. Via (Via-hole) design

Excessive via spacing can cause electromagnetic leakage. However, in real cases, vias cannot always be placed at minimum spacing or placed regularly, so the maximum spacing should be constrained based on the actual circuit board situation. Literature [32] suggests that the distance should be: $l < \frac{\lambda}{10} - \frac{\lambda}{100}$ (generally, $l < \frac{\lambda}{30}$), where *l* is the distance (m) and λ is the wavelength (m) [32]. To ensure good contact between the PCB and fixtures, edge via band design should also be considered [32].

3.3.2. Grounding

Grounding is another critical issue in PCB EMC design. Proper ground layer layout helps eliminate magnetic flux in multilayer PCBs, and a complete ground layer effectively reduces noise emissions across all frequency bands [33]. Here are several key principles of grounding:

3.3.2.1. Reduce ground line impedance

PCB ground impedance is a primary cause of radiated EMI, espicially for frequencies above 30 MHz [35]. Ground currents cause antenna effects when flowing through ground lines. Placing circuits with significant interference emissions closest to the confluence point reduces trace length and increases trace width [36], thereby limiting common impedance coupling by limiting noise circuit return path impedance. Additionally, copper plate on PCB ground planes reduces ground line impedance, enhances anti-interference capability [26]. A cross capacitor can be added between the output and input, and an impedance resonance network can be created to lower the ground impedance [36].

3.3.2.2. Ground plane position and design

For multilayer boards, a complete ground plane should be reserved in the PCB, with important signal lines adjacent to this layer, and it is better to put the ground layer loser to the clock source than to the antenna.

For projects with both digital and analog components, their grounds should be set separately (as shown in Figure.13) [35, 37]. Analog and digital grounds need to be connected, commonly through 0-ohm resistors, ferrite beads, inductors, capacitors, or A\D converters [37].



Figure 13: Ground setting [37]

4. Conclusion

This paper first reviews the sources of EMI in EVs, discussing their generation principles and propagation mechanisms. It also summarizes the current research in the field of PCB EMC design within EVs. An extensive evaluation of diverse EMI mitigation strategies was conducted for EV propulsion systems, encompassing tactics from diminishing noise origins to inhibiting propagation routes and optimizing PCB layouts. This analysis aimed to alleviate electromagnetic interference comprehensively. The successful implementation of these mitigation strategies is anticipated to significantly enhance the reliability, efficiency, and safety of EVs.

In recent years, the research on the electromagnetic interference mechanism of motor drive systems has gradually matured, and the research on EMC predictive modeling simulation and EMI suppression technology is still under development. Due to the EMI mechanism of the motor drive system and the complexity of the system, it brings great difficulties to accurate modeling. How to

accurately establish an EMI prediction simulation model of the motor drive system and effectively guide the engineering application is still an urgent problem that needs to be solved. In addition, the EMI suppression technology of the motor drive system is mainly used in practice. In the stage of laboratory research and exploration, a relatively complete solution has not been formed. How to comprehensively consider EMC characteristics in the process of product design and application, and develop corresponding design theories and specifications, which should be solved in future engineering applications.

References

- [1] IEA (2024), Global EV Outlook 2024, IEA, Paris https://www.iea.org/reports/global-ev-outlook-2024, Licence: CC BY 4.0
- [2] T. Jarin, P. V. Nisha, B. Deepanraj and H. Mewada, 'Comparison of PCB and Conventional Power Transfer Coils in Magnetic Coupler Designs for Electric Vehicles,' 2024 International Conference on Smart Systems for applications in Electrical Sciences (ICSSES), Tumakuru, India, 2024, pp. 1-6.
- [3] J. Yao, S. Wang and Z. Luo, 'Radiated EMI Reduction by Layout Improvement in Power Converters in Automotive Applications,' 2020 IEEE 9th International Power Electronics and Motion Control Conference (IPEMC2020-ECCE Asia), Nanjing, China, 2020, pp. 1894-1899.
- [4] D. Hamza, M. Pahlevaninezhad and P. K. Jain, "Implementation of a Novel Digital Active EMI Technique in a DSP-Based DC–DC Digital Controller Used in Electric Vehicle (EV)," in IEEE Transactions on Power Electronics, vol. 28, no. 7, pp. 3126-3137, July 2013, doi: 10.1109/TPEL.2012.2223764.
- [5] Songchun Zhang. Anti-interference technology for electronic control system and its application [M]. Beijing: China Machine Press 1998
- [6] Kuixuan Han. Introduction to Microwave Unified Measurement and Control System [M]. Beijing: National Defense Industry Press 1965
- [7] BoXue Tan. Principle and Application of Integrated Circuit [M]. Beijing: Publishing House of Electronics Industry 2003
- [8] P. Hemeng, H. Jianyao, J. Chunxu, L. Qunxing, X. Huawei and H. Zhiyuan, "Analysis for the EMI measurement and propagation path in Hybrid Electric Vehicle," 2016 IEEE Information Technology, Networking, Electronic and Automation Control Conference, Chongqing, China, 2016, pp. 1087-1090.
- [9] Zhai, L. (2021). EMI Prediction and Suppression of DC-DC Converter. In: Electromagnetic Compatibility of Electric Vehicle. Key Technologies on New Energy Vehicles. Springer, Singapore. https://doi.org/10.1007/978-981-33-6165-2_4
- [10] H. A. Huynh, Y. Han, S. Park, J. Hwang, E. Song and S. Kim, "Design and Analysis of the DC–DC Converter With a Frequency Hopping Technique for EMI Reduction," in IEEE Transactions on Components, Packaging and Manufacturing Technology, vol. 8, no. 4, pp. 546-553, April 2018
- [11] J. Ji, W. Chen and X. Yang, "Design and precise modeling of a novel Digital Active EMI Filter," 2016 IEEE Applied Power Electronics Conference and Exposition (APEC), Long Beach, CA, USA, 2016, pp. 3115-3120
- [12] Zhai, L. (2021). Electromagnetic Compatibility of Battery Management System. In: Electromagnetic Compatibility of Electric Vehicle. Key Technologies on New Energy Vehicles. Springer, Singapore. https://doi.org/10.1007/978-981-33-6165-2_7
- [13] D. Hamza, M. Pahlevaninezhad and P. K. Jain, 'Implementation of a Novel Digital Active EMI Technique in a DSP-Based DC–DC Digital Controller Used in Electric Vehicle (EV),' in IEEE Transactions on Power Electronics, vol. 28, no. 7, pp. 3126-3137, July 2013
- [14] Liang, C., Gu, Z., Zhang, Y. et al. Structural Design Strategies of Polymer Matrix Composites for Electromagnetic Interference Shielding: A Review. Nano-Micro Lett. 13, 181 (2021).
- [15] Sorgucu, U. Electromagnetic interference (EMI) shielding effectiveness (SE) of pure aluminum: an experimental assessment for 5G (SUB 6GHZ). J Mater Sci: Mater Electron 34, 2325 (2023).
- [16] Novák, M., Rosina, J., Bendová, H. et al. Low-cost and prototype-friendly method for biocompatible encapsulation of implantable electronics with epoxy overmolding, hermetic feedthroughs and P3HT coating. Sci Rep 13, 1644 (2023).
- [17] Yadav, A., Bera, T.K. Ferrite shielding thickness and its effect on electromagnetic parameters in wireless power transfer for electric vehicles (EVs). J. Eng. Appl. Sci. 70, 132 (2023).
- [18] Shen, X., Kim, JK. Graphene and MXene-based porous structures for multifunctional electromagnetic interference shielding. Nano Res. 16, 1387–1413 (2023).
- [19] Yang, J., Wang, H., Zhang, Y. et al. Layered Structural PBAT Composite Foams for Efficient Electromagnetic Interference Shielding. Nano-Micro Lett. 16, 31 (2024).

- [20] Lee, J.S., Kim, JW., Lee, J.H. et al. Flash-Induced High-Throughput Porous Graphene via Synergistic Photo-Effects for Electromagnetic Interference Shielding. Nano-Micro Lett. 15, 191 (2023).
- [21] Y. Zhang, J. Guo, H. Liu, X. Zhang, Y. Wang and Y. Fan, 'EMI Measurement and Reduction for SiC MOSFET based Motor Drivers of Electric Vehicles,' 2023 3rd International Conference on Electrical Engineering and Mechatronics Technology (ICEEMT), Nanjing, China, 2023, pp. 282-286
- [22] A. K. Ghose, S. K. Mandal and G. K. Deb, "PCB design with low EMI," 1995 International Conference on Electromagnetic Interference and Compatibility (INCEMIC), Madras, India, 1995, pp. 69-76, doi: 10.1109/IC EMIC.1995.501563.
- [23] C. R. Paul, Introduction to Electromagnetic Compatibility, John Wiley and Sons, 1992.
- [24] Chao Yang; Kun Yue; Thinking and analysis of PCB design process [J]. Technology and Innovation, 2023, (09): 153-155. DOI:10.15913/j.cnki.kjycx.2023.09.043
- [25] J. -M. Redouté and A. Richelli, 'A methodological approach to EMI resistant analog integrated circuit desig n,' in IEEE Electromagnetic Compatibility Magazine, vol. 4, no. 2, pp. 92-100, 2nd Quarter 2015, doi: 10.1 109/MEMC.2015.7204058.
- [26] Han Yang, and Tao Chen.' Automotive-grade PCB electromagnetic compatibility design.' Internal combustion engine and accessories .13(2018):11-14.doi:10.19475/j.cnki.issn1674-957x.2018.13.005.
- [27] Z. He and H. Guo, 'EMR Field Distribution Analysis of Crystal Oscillator on PCB, '2018 12th International Symposium on Antennas, Propagation and EM Theory (ISAPE), Hangzhou, China, 2018, pp. 1-4, doi: 10.11 09/ISAPE.2018.8634183.
- [28] M. Ali, J. Friebe and A. Mertens, "3-D Electromagnetic Modeling and Analysis of Electromagnetic Field Couplings of EMI Filter Capacitors," 2021 IEEE 12th Energy Conversion Congress & Exposition - Asia (ECCE-Asia), Singapore, Singapore, 2021, pp. 1299-1305, doi: 10.1109/ECCE-Asia49820.2021.9479282.
- [29] P. Kadlec, V. Šeděnka, M. Marek and M. Štumpf, "Optimizing a Decoupling Capacitor on a PCB: A Fully Time-Domain Approach Based on PSO and TD-CIM," 2018 International Symposium on Electromagnetic Compatibility (EMC EUROPE), Amsterdam, Netherlands, 2018, pp. 585-589, doi: 10.1109/EMCEurope.2018.8485008.
- [30] Shinichi Ikami and Akihisa Sakurai, 'Practical analysis on 20H rule for PCB, '2008 Asia-Pacific Symposium on Electromagnetic Compatibility and 19th International Zurich Symposium on Electromagnetic Compatibility, Singapore, 2008, pp. 180-183, doi: 10.1109/APEMC.2008.4559841.
- [31] F. Gisin and Z. Pantic-Tanner, 'Radiation from printed circuit board edge structures,'2001 IEEE EMC International Symposium. Symposium Record. International Symposium on Electromagnetic Compatibility (Cat. No.01CH37161), Montreal, QC, Canada, 2001, pp. 881-883 vol.2, doi: 10.1109/ISEMC.2001.950495.
- [32] Meishuang Chen, Sai Zhu, Lihua Cai, etal. Design for Integrated Circuit EMC Test PCB[J]. SAFETY&EMC, 2021(5):83-87
- [33] C. -H. Lee, C. -Y. Yao, H. -C. Li, D. -B. Lin and H. -P. Lin, "The study of PCB ground area and location on EMI reduction effectiveness," 2017 Progress in Electromagnetics Research Symposium Fall (PIERS FALL), Singapore, 2017, pp. 1568-1571, doi: 10.1109/PIERS-FALL.2017.8293382.
- [34] S. Haga, K. Nakano and O. Hashimoto, 'Reduction in radiated emission by symmetrical power-ground layer stackup PCB with no open edge, '2002 IEEE International Symposium on Electromagnetic Compatibility, Minneapolis, MN, USA, 2002, pp. 262-267 vol.1, doi: 10.1109/ISEMC.2002.1032486.
- [35] Z. Ma, S. Wang, Q. Huang and Y. Yang, 'A Review of Radiated EMI Research in Power Electronics Systems,' in IEEE Journal of Emerging and Selected Topics in Power Electronics, vol. 12, no. 1, pp. 675-694, Feb. 2024, doi: 10.1109/JESTPE.2023.3335972.
- [36] J. Yao, S. Wang, and Z. Luo, 'Modeling, analysis, and reduction of radiated EMI due to the voltage across input and output cables in an automotive non-isolated power converter,' IEEE Trans. Power Electron., vol. 37, no. 5, pp. 5455–5465, May 2022.
- [37] Ke Wu. Design optimization analysis of digital-analog hybrid PCB electromagnetic compatibility [J]. Integrated circuit applications, 2024, 41 (04): 39-41. DOI:10.19339/j.issn.1674-2583.2024.04.014.
- [38] W. Jiang, k. Cai, B. Sen and G. Wang, 'Practical High Speed PCB Stack up Tool Generation and Validation,' 2018 IEEE 68th Electronic Components and Technology Conference (ECTC), San Diego, CA, USA, 2018, pp. 2288-2294, doi: 10.1109/ECTC.2018.00344.